



PAPER

Impact of Ir doping on the thermoelectric transport properties of half-Heusler alloys

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E-mail: zoulikha@gmail.com, zoulikha.charifi@univ-msila.dz, rabah_khenata@univ-mascara.dz and khenata_rabah@yahoo.fr**Keywords:** Half Heusler alloys, Boltzmann, seebeck coefficient, thermoelectric performance**Abstract**

Using density functional and Boltzmann transport theories, we investigate the thermoelectric transport properties $\text{ZrCo}_{1-x}\text{Ir}_x\text{Sb}$ ($x = 0, 0.125, 0.25, 0.375, 0.5, 0.625, 0.75, 0.875, 1$) half-Heusler alloys. The current work found that increasing the concentration of iridium (Ir_x) from $x = 0$ to 0.375 in the $\text{ZrCo}_{1-x}\text{Ir}_x\text{Sb}$ alloys from room temperature to 800 K significantly decreased thermal and electrical conductivity due to a shorter relaxation time. Furthermore, our results show that $\text{ZrCo}_{0.625}\text{Ir}_{0.375}\text{Sb}$ has the highest Seebeck coefficient ($353.93 \mu\text{V/K}$) at 300 K, thereby boosting its thermoelectric performance. Interestingly, the thermoelectric figure of merit (ZT) has exceptional value 1.01 by applying 25% ($x = 0.25$) of atomic doping of iridium (Ir) with a carrier concentration of $n = 1.47 \cdot 10^{20} \text{ cm}^{-3}$ at 1000 K and 37.5% ($x = 0.375$) of atomic doping of iridium (Ir) with a carrier concentration of $n = 7.23 \cdot 10^{19} \text{ cm}^{-3}$ at 800 K. Calculations present important results on the suitability of the studied alloys for thermoelectric applications.

1. Introduction

Developing methods for converting renewable energy is an efficient solution to address the energy issue, as the world's energy demands are rising, and fossil fuel supplies are running out. Thermoelectric materials are highly beneficial for cooling and heat energy-collecting applications because they are green energy resources. They can directly convert heat energy into electrical energy through the thermoelectric effect.

By utilizing thermoelectric (TE) materials, thermal waste recovery offers a viable approach to generating power that is dependable, sustainable, and expandable through the utilization of waste thermal energy [1, 2]. A thermoelectric device's conversion efficiency is highly dependent on the dimensionless figure of merit ($ZT = S^2\sigma T/\kappa$) of the materials, which S stands for the Seebeck coefficient, σ electrical conductivity, and κ thermal conductivity [3]. T indicates the absolute temperature. The two components of thermal conductivity are the electronic contribution (κ_e) and the lattice vibration contribution (κ_l), where the power factor ($S^2\sigma$) is defined. Nevertheless, the various parameters entering ZT are coupled, so increasing thermoelectric efficiency is not a simple task. Therefore, the task is to find novel compounds and maximize their ZT values by enhancing phonon scattering and maximizing carrier concentration.

Half-Heusler (HH) compounds have garnered significant attention in recent years owing to their thermal stability, high power factor [4–7], cost-effectiveness, and non-toxicity. Research has shown considerable interest in the ZrCoSb and ZrNiSn types of HH alloys. Like other thermoelectric materials, there are two fundamental techniques for boosting the ZT of half-Heusler alloys: lowering their thermal conductivity and raising the power factor. Improving these two TE attributes simultaneously can be difficult because of their relationship. In addition, many other techniques, including point defect scattering [8], nanostructuring [9], phase separation [10], band engineering [11], and plastic deformation, have been used besides carrier concentration optimization to enhance the thermoelectric performance of the half-Heusler compounds. [12]. Highly doped semiconductors

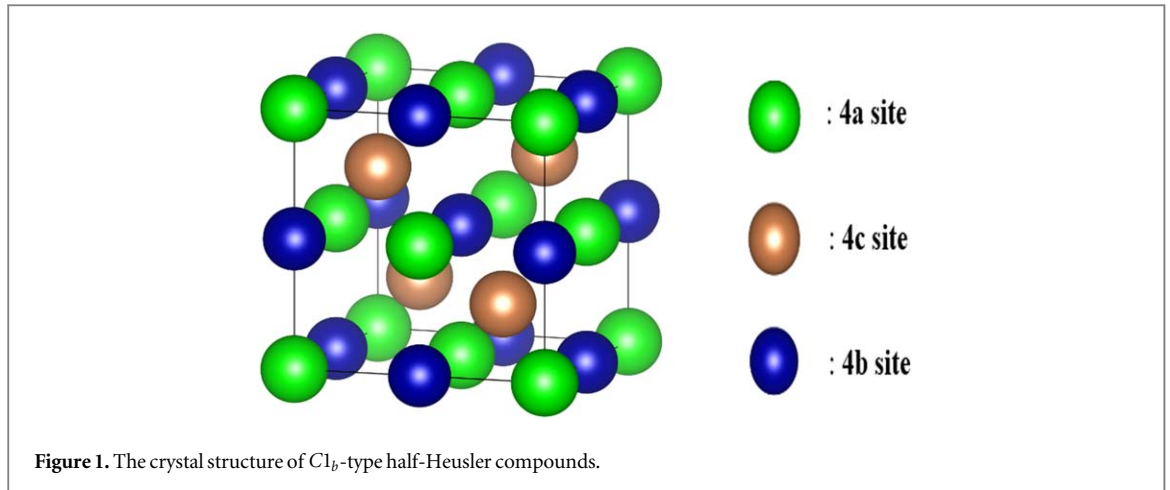
with a carrier concentration of about $10^{18} - 10^{20}$ carriers cm^{-3} are suitable thermoelectric materials [13]. There are various conceivable combinations for forming HH [14, 15] alloys, including ZrCoSb [16–18] (p-type), TiCoSb [19] (p-type), ZrNiSn [20–24] (n-type), and TiNiSn [25, 26] (n-type), which have been extensively investigated. Although $ZT > 1$ has already been achieved in n-type HH.

In terms of theory, Yang *et al* [27] estimated the ideal doping concentrations for each of the ternary half-Heusler compounds by computing the electronic transport properties of numerous semiconducting ternary half-Heusler compounds, such as ZrCoSb and TiCoSb, using *ab initio* calculations and the Boltzmann transport equation. Shen *et al* [28] determined the implication of partial nickel substitution with palladium on the thermoelectric properties of ZrNiSn-based half-Heusler compounds and discovered that substituting palladium for nickel leads to a significant, good decrease in thermal conductivity. The study was conducted by Dinesh C. Gupta and Gurunani Bharti [29]. They found that for the CoZrSi and CoZrGe Heusler alloys, the measured ZT values at 900 K are 0.51 and 0.57, respectively. On the other hand, these two authors indicate that half-Heusler alloys based on rhodium have the potential to be used in thermoelectric applications over a wide temperature range [30]. The carrier concentration is optimum at 10^{19} cm^{-3} . In his 2019 paper, D.M. Hoat demonstrated that TaRhSn (Pb) has a higher thermopower than TaRuSb (Bi) because of their denser electronic states close to the Fermi level. With a maximum chemical potential of around -0.25 eV , these materials exhibit a high power factor (PF) in the p-region [31]. According to a theoretical study of the two half-Heusler alloys, KCrSi and KCrGe, carried out by Gurunani *et al* [32], the high figure of merit ZT at 900K is produced by the alloys' poor thermal conductivity and high Seebeck coefficient.

On the experimental side, the maximum power factor for TiCoSb-based alloys is $23 \mu\text{Wcm}^{-1}\text{K}^{-2}$ at 850K, as determined by the experiment [33]. According to estimates from Xia, Yu, *et al* [34] at 300K, resistivity ρ drops from $\sim 5 \times 10^4 \mu\Omega \text{ cm}$ in the undoped phase to $1 - 2 \times 10^3 \mu\Omega \text{ cm}$ in the substituted phases, while the Seebeck coefficient S for ZrCoSb reaches -110 and $+130 \mu\text{V/K}$. Mitra, Mousumi, *et al* [35] confirmed experimentally that doping with as little as ~ 0.3 atomic percent aluminum (Al) can significantly improve the thermoelectric properties of $\text{Hf}_{0.3}\text{Zr}_{0.7}\text{Co}(\text{Sn}_{0.3}\text{Sb}_{0.7})_{1-x}\text{Al}_x$ Half Heusler alloy. $\text{Zr}_{1-x}\text{Hf}_x\text{CoSb}_{0.9}\text{Sn}_{0.1}$ alloys are intriguing prospects for mid-temperature power generation applications because of their improved ZT due to Hf-substitution, which has been experimentally accomplished to achieve a very low thermal conductivity (Chauhan *et al* [36]). He *et al*'s research study [37] demonstrates that phonon scattering occurs when Sn substitutes at the Sb sites in half-Heusler compounds ZrCoSb. Regarding the need for a more thorough comprehension of phonon transport for half-Heusler compounds to facilitate further material optimization and improve their thermoelectric performance, this result also holds for a large class of HH compounds, including ZrNiSn, ZrCoBi, and NbFeSb. The thermoelectric performance of the HH compounds is better than that of many current thermoelectric materials.

Using thermoelectric applications to recover electrical energy from waste heat improves the efficiency of heat-to-electricity systems. The need for better-performing, higher-temperature TE materials than those now in use is driving growing interest in this field due to the proposed industrial and military applications of TE materials. In recent years, there has been research on the application of TEs in TE-solar. A few examples of novel use for thermoelectrics (TEs) are biothermal batteries for cardiac pacemakers and radioisotope TE generators for deep-space probe power. Furthermore, TE refrigeration applications include the manufacturing of refrigeration systems, refrigerators, seat coolers for electrically powered cooling and relaxation, and the cooling of electrical components. The TE domain has gained multidisciplinary interest, and the worldwide TE market has risen due to these encouraging developments.

In our previous study, we investigated the structural, electronic, and mechanical properties of $\text{ZrCo}_{1-x}\text{Ir}_x\text{Sb}$ half-Heusler alloys across a range of iridium concentrations ($x = 0, 0.125, 0.25, 0.375, 0.5, 0.625, 0.75, 0.875$, and 1). The findings are published in the article titled 'Iridium's influence on the structural, electronic and mechanical characteristics of $\text{ZrCo}_{1-x}\text{Ir}_x\text{Sb}$ half-Heusler alloys' [38]. We evaluated the exchange–correlation (XC) energy using the local density (LDA) and generalized gradient (GGA) approximations. Our findings showed that increasing Ir atom concentration leads to an enlargement of the lattice constant (from 6.10 to 6.36 Å) and bulk modulus (from 138.09 to 149.70 GPa), which result in increased volume and hardness of the compound. The energy band structure was determined using EV-GGA and mBJ-GGA. These methods were employed to improve the accuracy of the band structure and density of states calculations. Our findings indicated that the alloys exhibit semiconductor characteristics with both direct and indirect band gaps, depending on the iridium concentration. Specifically, alloys with $x = 0.75$ and $x = 0.875$ exhibited a direct band gap, while other concentrations showed an indirect band gap. The calculated band gap energies were in good agreement with previous theoretical predictions, further validating our approach. Moreover, we computed the elastic constants and determined mechanical stability, bulk modulus, shear modulus, Young's modulus, Poisson's ratio, hardness, anisotropy factor, sound velocities, and Debye temperature using VRH approximations. These results provide a comprehensive understanding of the structural and elastic properties of $\text{ZrCo}_{1-x}\text{Ir}_x\text{Sb}$ alloys, supporting their potential for thermoelectric applications.



Our objective in this work is to investigate the thermoelectric properties of half-Heusler alloys, specifically aiming to identify compounds with a high thermoelectric figure of merit (ZT) and enhanced performance. We focus on varying the concentration of iridium in the $\text{ZrCo}_{1-x}\text{Ir}_x\text{Sb}$ ($x = 0, 0.125, 0.25, 0.375, 0.5, 0.625, 0.75, 0.875, 1$) alloy to achieve this goal.

This study intends to investigate the Boltzmann semiclassical transport equation and constant relaxation time approximation is used to calculate thermoelectric properties, which are implemented in the BoltzTrap code. The Seebeck coefficient, electrical conductivity, thermal conductivity (lattice vibration contribution and electronic contribution), and the figure of merit are calculated versus carrier concentrations at various temperatures. The order of the paper is as follows: The computing process is briefly explained in section 2, and the Boltzmann equation is used to construct the transport coefficients. Section 3 describes the results of $\text{ZrCo}_{1-x}\text{Ir}_x\text{Sb}$ ($x = 0, 0.125, 0.25, 0.375, 0.5, 0.625, 0.75, 0.875, 1$) HH alloys. Finally, section 4 provides a summary of the work's significant findings.

2. Computational details

To achieve the targeted alloy compositions with x values of 0.25, 0.50, 0.75, and 1, we employed a substitution approach where cobalt (Co) atoms were replaced by iridium (Ir) atoms in a unit cell that contains four atoms. Specifically, one, two, three, and four Co sites were substituted with Ir in this configuration. For alloys with x values of 0.125, 0.375, 0.625, and 0.875, the substitution involved one, three, five, and seven Co sites, respectively, within a larger supercell comprising eight atoms. During this process, we accounted for the valence electron configurations of Zr ($[\text{Kr}] 4d^2 5s^2$), Co ($[\text{Ar}] 3d^7 4s^2$), Ir ($[\text{Xe}] 4f^{14} 5d^7 6s^2$), and Sb ($[\text{Kr}] 4d^{10} 5s^2 5p^3$). The remaining electron configurations were considered as core states.

Figure 1 illustrates the crystal arrangement of $C1_b$ -type half-Heusler (HH) alloys, which includes three distinct atomic positions: 4a (0, 0, 0), 4b (0.5, 0), and 4c (0.25, 0.25, 0.25). The crystallographic positions of 4a and 4b can be interchanged. To evaluate this, three structural configurations were analyzed where one of the components occupies the 4c site while the remaining two are situated at the 4a and 4b sites. Lattice parameters for these configurations were optimized using density functional theory (DFT). The stability of these configurations was assessed by comparing their total energies, with the most stable model being the one with the lowest total energy. The DFT calculations were carried out using the WIEN2K software [39]. Band structures were computed employing various methods, including the EV-GGA [40] and mBJ-GGA [41] approximations.

To assess the thermoelectric performance of our material, we calculated the figure of merit (ZT), a key indicator of efficiency in converting thermal energy to electrical energy. This calculation involves several critical transport properties.

We used the semi-classical Boltzmann theory, implemented through the BoltzTraP code [42], to determine the Seebeck coefficient, which measures the voltage generated by a temperature gradient. Electrical conductivity and electronic thermal conductivity were also calculated using the same code, applying a constant relaxation time approximation for consistency [43]. For lattice thermal conductivity, which reflects heat transport via lattice vibrations, we employed Slack's empirical equations and further refined our estimates using the Gibbs2 code [44–47]. This code incorporates thermodynamic parameters such as the Debye temperature and Grüneisen parameter, which are essential for accurate predictions. The total thermal conductivity was computed by summing the electronic and lattice thermal conductivities. This comprehensive value is crucial for evaluating the material's overall thermal performance. The figure of merit (ZT) was then calculated using these properties,

providing a measure of the material's ability to convert waste heat into usable electrical energy. A figure of merit (ZT) is a numerical expression representing the efficiency of a given material. Once all transport coefficients have been obtained, a method to assess the thermoelectric performance of half-Heusler alloys is by calculating the ZT value, which can be expressed as: $ZT = \frac{S^2 \sigma T}{k_{tot}}$. The constant relaxation time is taken to be $\tau = 2.10^{-14}$ s, in this equation, the temperature (T) is related to the total thermal conductivity (k_{tot}), which is made up of the sum of the electronic (k_e) and lattice (k_L) thermal conductivity. The Seebeck coefficient (S) and electrical conductivity (σ) are also involved.

3. Results and discussion

3.1. Thermoelectric transport properties

Scientists are driven by the growing need for energy to explore new materials and devices that can efficiently convert thermal energy into electrical power. Materials possessing thermoelectric (TE) properties can be applied in this particular context. These compounds can harness the Seebeck or Peltier phenomenon, which is helpful for generating electrical power. TE materials have a wide range of potential applications in energy devices.

3.1.1. Lattice thermal conductivity

One of a solid's most basic physical properties is its thermal conductivity, which significantly affects a compound's thermal performance. For many years, various theoretical approaches have been used to study the lattice thermal conductivity k_l of semiconductor materials [48–54]. The lattice thermal conductivity k_l refers to the conduction of heat through the vibrations of the lattice ions within a solid. Research into the physics underlying the heat-conduction process has fundamentally enabled a thorough understanding of the nature of lattice vibrations in solids. Weak lattice thermal conductivity is a necessary characteristic for possible thermoelectric materials. The Slack's equation [55, 56] is a commonly used approximation for calculating lattice thermal conductivity:

$$k_l = A \cdot \frac{\bar{M}_a \theta_D^3 \delta}{\gamma^2 T n^{2/3}}. \quad (1)$$

In which A is a constant having the following value: $A = 3.04 \times 10^{-8}$, \bar{M}_a is the average atomic mass of the crystal, δ^3 is the average volume of just one atom, γ is the Grüneisen parameter, and explicates the crystalline material's anharmonic properties [57], T is the temperature, and n represents the total number of atoms in the primitive unit of a cell.

Since the BoltzraP code computes all transport properties but lattice thermal conductivity k_l (which includes Debye temperature θ_D in its formula), we are forced to apply the Gibbs code to compute Debye temperature θ_D , which is the basis for deriving k_l . Understanding the Gibbs free energy $G(x; p; T)$ is crucial for analyzing the shape and stability of a solid under specific temperature and pressure conditions using the quasi-harmonic approximation. It can be written as

$$G(x; p; T) = E(x) + pV(x) + A_{vib}(x; T). \quad (2)$$

When considering the crystal's total energy $E(x)$, it is essential to consider the variables of the pressure p and the volume $V(x)$. The vibrational Helmholtz free energy is represented by $A_{vib}(x; T)$. The formula for this is as follows:

$$A_{vib}(x; T) = \int_0^\infty \left[\frac{\hbar\omega}{2} + K_B T \ln(1 - e^{-\frac{\hbar\omega}{K_B T}}) \right] g(x; \omega) d\omega \quad (3)$$

where K_B Boltzmann's constant $g(x; \omega) d\omega$ is the phonon density of states. We can mention the vibrational Helmholtz free energy as a function of Debye temperature θ_D by using the Debye model for the phonon density of states, which accounts for the vibrational contribution. It's stated as such:

$$A_{vib}(\theta; T) = nK_B T \left[\frac{9}{8} \frac{\theta}{T} + 3 \ln(1 - e^{-\theta/T}) - D\left(\frac{\theta}{T}\right) \right]. \quad (4)$$

In which $D\left(\frac{\theta}{T}\right)$ denotes the Debye integral, which can be defined as

$$D\left(\frac{\theta}{T}\right) = 3 \left(\frac{T}{\theta}\right)^3 \int_0^{\theta/T} \frac{x^3}{e^x - 1} dx. \quad (5)$$

Table 1. Debye temperature θ_D , The Volume δ , the average Gruneisen parameter γ and lattice thermal conductivity k_L at 300 K, 600 K, and 900 K for $\text{ZrCo}_{1-x}\text{Ir}_x\text{Sb}$ ($x = 0, 0.125, 0.25, 0.375, 0.5, 0.625, 0.75, 0.875, 1$) half heusler compounds.

Compounds	T (K)	θ_D (K)	δ (bohr ³)	γ	k_L (W/m.K)
ZrCoSb	T = 300 K	390	388.2395	2.2670522	13.46175
	T = 600 K	380.2	392.5899	2.2994247	6.08432
	T = 900 K	369.54	397.4335	2.3372204	3.61979
ZrCo _{0.875} Ir _{0.125} Sb	T = 300 K	383.61	3156.4356	1.9821934	4.47003
	T = 600 K	376.56	3185.9342	2.0030573	2.07666
	T = 900 K	369.05	3217.9839	2.02649	1.27753
ZrCo _{0.75} Ir _{0.25} Sb	T = 300 K	374.24	1609.9521	2.1857597	5.7693
	T = 600 K	365.99	1626.3481	2.21286	2.64129
	T = 900 K	357.12	1644.3585	2.2438642	1.59686
ZrCo _{0.625} Ir _{0.375} Sb	T = 300 K	369.42	3281.2402	2.2703441	3.40421
	T = 600 K	360.95	3314.6958	2.29976	1.55257
	T = 900 K	351.82	3351.5454	2.33358	0.93433
ZrCo _{0.5} Ir _{0.5} Sb	T = 300 K	362.11	830.26	2.18066	9.3408
	T = 600 K	354.61	838.2219	2.20598	4.2997
	T = 900 K	346.58	846.9134	2.2347031	2.61674
ZrCo _{0.375} Ir _{0.625} Sb	T = 300 K	356.93	3379.667	2.2117694	3.60549
	T = 600 K	349.54	3411.5779	2.2374263	1.65966
	T = 900 K	341.64	3446.3891	2.2665065	1.01017
ZrCo _{0.25} Ir _{0.75} Sb	T = 300 K	351.8	1709.459	2.3424518	5.18644
	T = 600 K	343.8	1726.2255	2.3728045	2.36646
	T = 900 K	335.19	1744.6459	2.4076051	1.42513
ZrCo _{0.125} Ir _{0.875} Sb	T = 300 K	347.64	3471.2022	2.2351931	3.61178
	T = 600 K	340.67	3502.5922	2.2602781	1.66691
	T = 900 K	333.24	3536.7201	2.2885779	1.01786
ZrIrSb	T = 300 K	340.44	439.1815	2.4207408	12.19377
	T = 600 K	332.45	443.4835	2.45357	5.54466
	T = 900 K	323.83	448.2178	2.49134	3.32524

It is assumed that an isotropic solid is used to compute the Debye temperature.

$$\theta = \frac{\hbar}{K_B} [6\pi^2 V^{1/3} n]^{1/3} f(\sigma) \sqrt{\frac{B_s}{M}}. \quad (6)$$

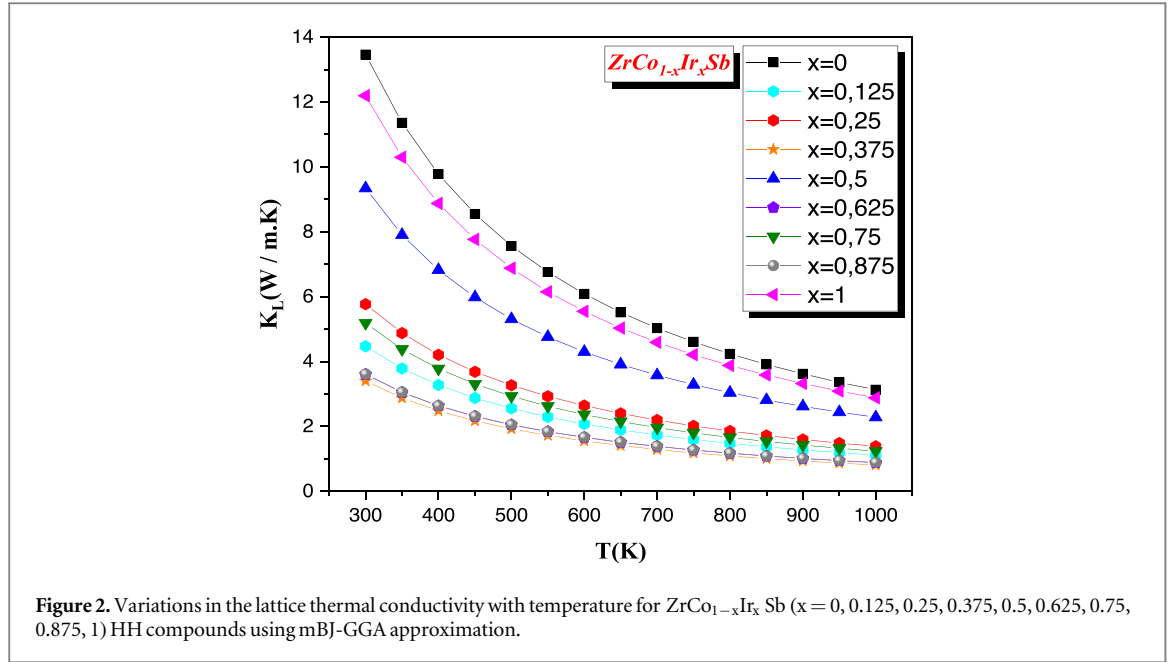
where σ is the Poisson ratio, B_s is the adiabatic bulk modulus, M is the molecular mass per formula unit, and $f(\sigma)$ is determined by

$$f(\sigma) = \left\{ 3 \left[2 \left(\frac{2}{3} \frac{1+\sigma}{1-2\sigma} \right)^{3/2} + \left(\left(\frac{1}{3} \frac{1+\sigma}{1-\sigma} \right)^{3/2} \right) \right]^{-1} \right\}^{1/3}. \quad (7)$$

The material exhibits a low lattice thermal conductivity at low Debye temperatures, along with high Grüneisen parameters and volume, as demonstrated in table 1 and figure 2. In figure 2, the lattice thermal conductivity of all HH alloys shows a decreasing trend with temperature. The compound $\text{ZrCo}_{0.625}\text{Ir}_{0.375}\text{Sb}$ exhibits a significantly low value of lattice thermal conductivity. This explains why the Grüneisen parameter of this compound exhibits high values at elevated temperatures. The experimental study was conducted by Bahrami, Amin, *et al* [58]. Half-Heusler compounds demonstrate the potential of cryomilling in decreasing lattice thermal conductivity and enhancing thermoelectric performance by enhancing phonon scattering. The research conducted by Verma, Ajay Kumar, *et al* [59] also highlights the effectiveness of generating significant point defects through heavy isovalent substitution in reducing phonon transport in Half-Heusler alloys. Researchers have demonstrated how manipulating entropy can significantly enhance the thermoelectric performance of an Hf-free half-Heusler compound, resulting in a remarkable reduction in lattice thermal conductivity.

3.1.2. Transport properties

This section will explore the thermoelectric properties of $\text{ZrCo}_{1-x}\text{Ir}_x\text{Sb}$ half Heusler alloys at nine different concentrations, ranging from 0 to 1. All the necessary calculations have been performed to determine the Seebeck coefficient S , electrical conductivity σ , thermal electronic conductivity k_e , and thermoelectric figure of merit ZT . When these parameters are at their optimal values, the dimensionless figure of merit can be maximized. These parameters are interconnected. Therefore, changing just one or two factors will not lead to a



significant increase in value. These properties, calculated from the semi-classical Boltzmann transport equation using the rigid band approximation and constant relaxation time approximation, are sufficient for characterizing a material's efficiency in thermoelectric energy applications [60].

3.1.2.1. Seebeck coefficient

The Seebeck effect and potential difference occur when two dissimilar conductors or semiconductors are brought into contact at different temperatures. This results in the movement of free electrons from the region with a higher temperature to the area with a lower temperature. The electromotive force between these two materials is determined by the temperature difference between the two junctions and the chemical composition of the compounds. Enhanced thermoelectric devices require significant Seebeck coefficients. The Seebeck coefficient measures the magnitude of the thermoelectric effect, which is the generation of an electric voltage in a material due to a temperature difference across it.

$$S = eK_B\sigma^{-1}\sum_k\left(-\frac{\partial f_0}{\partial E}\right)\tau_{\vec{k}}v_{\vec{k}}v_{\vec{k}}\left(\frac{\varepsilon_{\vec{k}}-\mu}{K_BT}\right). \quad (8)$$

where μ the chemical potential ε_k is the band energy.

As seen in figure 3(a), these alloys have Seebeck coefficients greater than 200 $\mu\text{V/K}$ except for composition $x = 0.875$, whose Seebeck value is higher than 200 $\mu\text{V/K}$ above the temperature of 550 K, and according to other authors' earlier research, high-performance thermoelectric materials are those having a Seebeck coefficient more significant than 200 $\mu\text{V/K}$ [61]. Even at room temperature, we can see that three alloys with concentrations of $x = 0.125$, $x = 0.375$, and $x = 0.625$ have Seebeck coefficients higher than 300 $\mu\text{V/K}$. Of these, $\text{ZrCo}_{0.625}\text{Ir}_{0.375}\text{Sb}$ it has the highest Seebeck coefficient of 353.93 $\mu\text{V/K}$, while $\text{ZrCo}_{0.875}\text{Ir}_{0.125}\text{Sb}$ and $\text{ZrCo}_{0.375}\text{Ir}_{0.625}\text{Sb}$ has Seebeck coefficients of 341.13 $\mu\text{V/K}$ and 318.66 $\mu\text{V/K}$, respectively. Along with these three alloys ($x = 0.125$, $x = 0.375$, and $x = 0.625$), we also observed that for the alloy with concentration $x = 0.75$, the maximum value S decreases with increasing temperature. Regarding alloys ZrCoSb , $\text{ZrCo}_{0.75}\text{Ir}_{0.25}\text{Sb}$, $\text{ZrCo}_{0.5}\text{Ir}_{0.5}\text{Sb}$, and ZrIrSb , the Seebeck value rises with temperature until 600 K, when it achieves its highest value of 235.44 $\mu\text{V/K}$, 285.57 $\mu\text{V/K}$, 226.74 $\mu\text{V/K}$, and 294.95 $\mu\text{V/K}$, respectively. Above this temperature, the Seebeck values start to drop. Finally, for $\text{ZrCo}_{0.125}\text{Ir}_{0.875}\text{Sb}$, the Seebeck value increases with increasing temperature until it hits its peak at 800 K, which is 218.87 $\mu\text{V/K}$, and then begins to fall above this point.

Figure 3(b) presents the Seebeck coefficient (S) as a function of chemical potential for $\text{ZrCo}_{1-x}\text{Ir}_x\text{Sb}$ half-Heusler (HH) alloys at a fixed temperature of 900 K. The plot reveals that each alloy exhibits two distinct peaks in the Seebeck coefficient, indicating regions where the thermoelectric performance is particularly enhanced. For the $\text{ZrCo}_{0.125}\text{Ir}_{0.875}\text{Sb}$ alloy, these peaks are most pronounced, with extreme values occurring between 0.12 eV and 0 eV. This behavior suggests significant asymmetry in the density of states around the Fermi level, which in turn affects carrier distribution. The positive peak corresponds to the dominance of holes as the primary charge carriers, while the negative peak reflects the dominance of electrons. The presence of both peaks indicates that

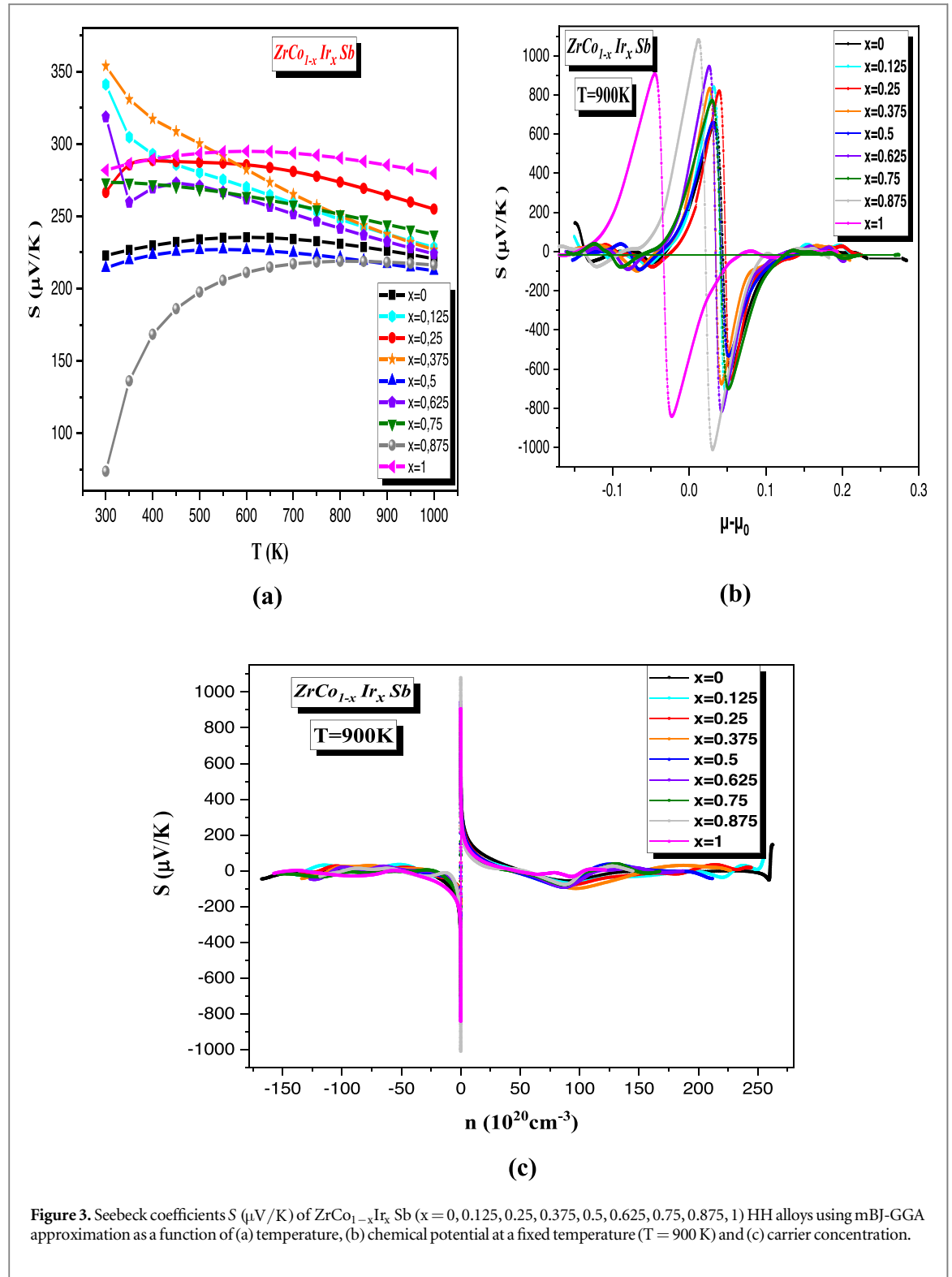


Figure 3. Seebeck coefficients S ($\mu\text{V/K}$) of $\text{ZrCo}_{1-x}\text{Ir}_x\text{Sb}$ ($x = 0, 0.125, 0.25, 0.375, 0.5, 0.625, 0.75, 0.875, 1$) HH alloys using mBJ-GGA approximation as a function of (a) temperature, (b) chemical potential at a fixed temperature ($T = 900\text{ K}$) and (c) carrier concentration.

the alloy can be tuned for either p-type or n-type thermoelectric applications depending on the chemical potential, thus offering flexibility in device design.

In figure 3(c), the computed Seebeck coefficients (S) are plotted against carrier concentration at various concentrations and a constant temperature of $T = 900\text{ K}$. The figure clearly shows that for all alloys, the Seebeck coefficient decreases as the carrier concentration increases. This trend is expected, as a higher carrier concentration typically leads to a decrease in the thermoelectric power due to the reduction in the energy difference between the carriers and the Fermi level. However, it is noteworthy that the Seebeck coefficient reaches its maximum value of $1080\text{ }\mu\text{V/K}$ for the $\text{ZrCo}_{0.125}\text{Ir}_{0.875}\text{Sb}$ alloy when the carrier concentration is zero. This maximum value highlights the potential of this alloy for applications requiring high thermoelectric efficiency at low carrier concentrations. Beyond this point, as the carrier concentration increases, the Seebeck

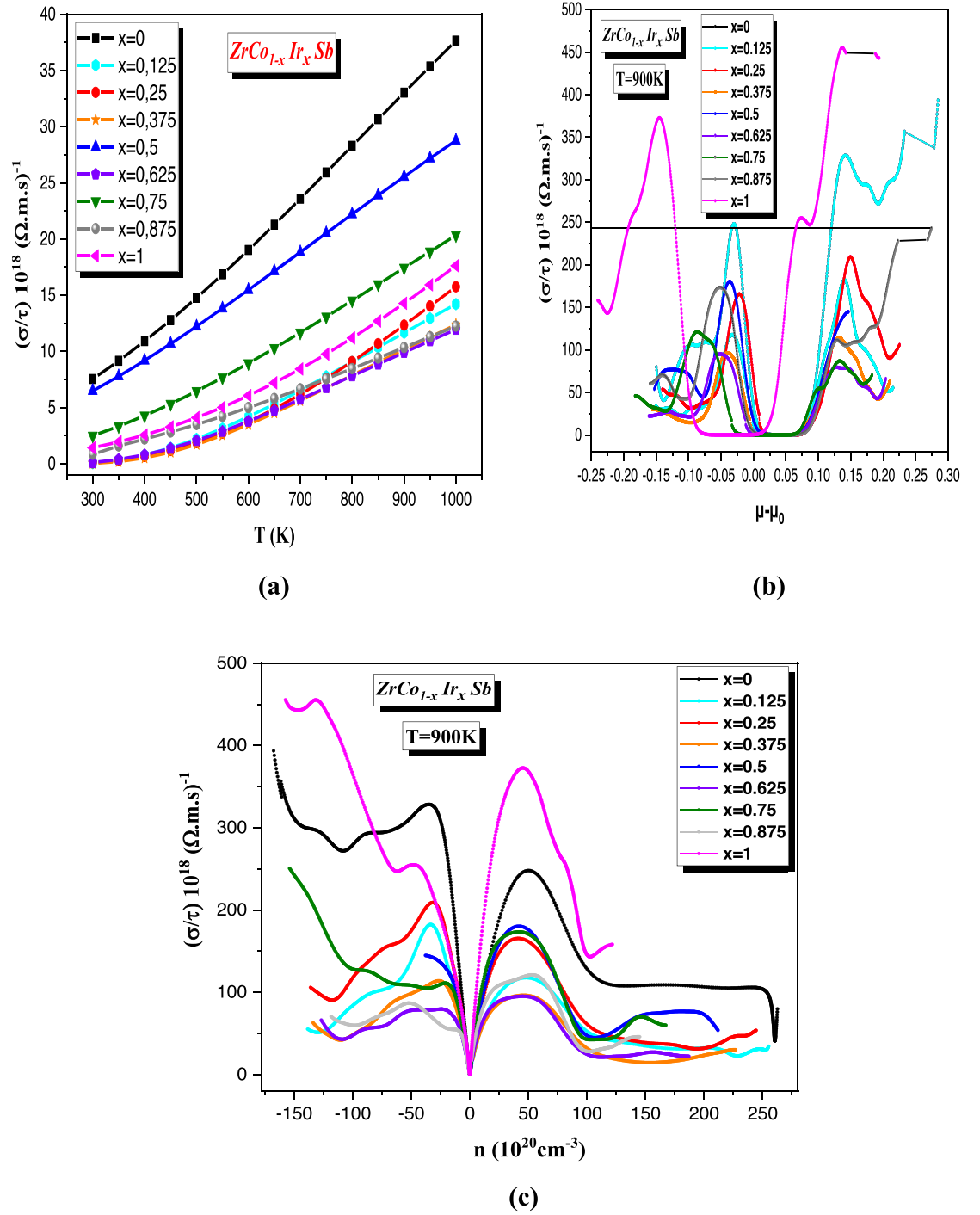


Figure 4. Electrical conductivity $(\sigma/\tau)10^{18} (\Omega \cdot \text{m} \cdot \text{s})^{-1}$ of $\text{ZrCo}_{1-x}\text{Ir}_x\text{Sb}$ ($x = 0, 0.125, 0.25, 0.375, 0.5, 0.625, 0.75, 0.875, 1$) HH alloys using mBJ-GGA approximation as a function of (a) temperature, (b) chemical potential at a fixed temperature ($T = 900 \text{ K}$) and (c) carrier concentration.

coefficient begins to decline for all alloys, eventually approaching zero. This decline can be attributed to the increased scattering and lower energy separation between carriers, reducing the ability of the material to maintain a high thermoelectric voltage. The behavior underscores the importance of optimizing carrier concentration to maximize the Seebeck coefficient and, by extension, the thermoelectric performance of the material.

3.1.2.2. Electrical conductivity

The mobility of free charge carriers in a thermoelectric compound generates electrical conductivity due to the thermoelectromotive force; hence, a better thermoelectric material must have a high electrical conductivity that lowers the Joule heating effect [62]. The following expression describes electrical conductivity.

$$\sigma = e^2 \sum_k \left(-\frac{\partial f_0}{\partial E} \right) \tau_{\vec{k}} v_{\vec{k}} v_{\vec{k}}. \quad (9)$$

where electrical conductivity is denoted by σ , A Fermi distribution function is represented by f_0 . $\tau_{\vec{k}}$ and $v_{\vec{k}}$ separately illustrate the relaxation time and group velocity associated with the \vec{k} state.

Plotting the electrical conductivity $(\sigma/\tau)10^{18} (\Omega.m.s)^{-1}$ for $ZrCo_{1-x}Ir_xSb$ HH alloys (where τ is the relaxation time) with temperature (T) in the range of 300 to 1000 K is shown in figure 4(a). As seen in figure 4(a), the electrical conductivity of all alloys increased linearly with temperature. On the other hand, we found that at room temperature, the electrical conductivity of alloys with concentrations of ($x = 0.125, 0.25, 0.375, 0.625$, and 0.875) is almost null $(\sigma/\tau) \sim 0$. Furthermore, a maximum electrical conductivity value of $37.65 \times 10^{18} (\Omega.m.s)^{-1}$ at 1000 K was determined for the ternary alloy $ZrCoSb$, which is higher than the other alloys. Additionally, two maximum values above $20 \times 10^{18} (\Omega.m.s)^{-1}$ were estimated for $ZrCo_{0.5}Ir_{0.5}Sb$ alloy and $ZrCo_{0.25}Ir_{0.75}Sb$ alloy at the same temperature (1000 K), $28.77 \times 10^{18} (\Omega.m.s)^{-1}$ and $20.32 \times 10^{18} (\Omega.m.s)^{-1}$, respectively.

Figure 4(b) illustrates the variation in electrical conductivity (σ/τ) as a function of chemical potential (μ) for $ZrCo_{1-x}Ir_xSb$ half-Heusler (HH) alloys at a constant temperature of 900 K. The figure demonstrates that for all alloys, electrical conductivity increases as the chemical potential moves away from the Fermi level, reaching an optimum value of $372.56 \times 10^{18} (\Omega.m.s)^{-1}$ at a chemical potential of -0.14 eV for the $ZrIrSb$ alloy. This increase suggests an enhanced carrier density or mobility as the chemical potential deepens into the valence band, facilitating greater electrical conductivity. However, as the chemical potential approaches 0 eV, corresponding to the Fermi level, the electrical conductivity sharply declines, reaching a minimum value of $0.00168 \times 10^{18} (\Omega.m.s)^{-1}$, also for the $ZrIrSb$ alloy. At this point, σ/τ effectively becomes zero, indicating that the availability of charge carriers is significantly reduced, as the energy states at the Fermi level are fully occupied in the valence band and only sparsely populated in the conduction band. Beyond the Fermi level, as the chemical potential continues to rise, electrical conductivity begins to increase again, reflecting the thermal excitation of electrons into the conduction band, which restores the material's conductivity. This behavior highlights the complex interplay between chemical potential and electronic structure in determining the electrical properties of these alloys, suggesting that fine-tuning the chemical potential could be key to optimizing electrical performance for thermoelectric applications.

Figure 4(c) depicts the variation in electrical conductivity (σ/τ) as a function of carrier concentration for the $ZrCo_{1-x}Ir_xSb$ HH alloys. The plot shows that the $ZrIrSb$ alloy exhibits the highest electrical conductivity at a carrier concentration of $45.81 \times 10^{20} cm^{-3}$ in the negative carrier concentration region. This indicates that at this particular concentration, the alloy's charge carriers are optimally positioned within the band structure to facilitate maximum electrical transport. However, as the carrier concentration approaches the Fermi level, the electrical conductivity for all alloys decreases, eventually reaching zero. This reduction is likely due to increased scattering and reduced mobility as carrier concentration increases, particularly near the Fermi level where the balance between available states and carrier energy levels is most delicate. The observed decline to zero conductivity at the Fermi level further underscores the importance of carrier concentration in controlling the material's electrical properties. These insights provide a valuable framework for optimizing doping levels and engineering the electronic structure to achieve desirable electrical conductivity, especially for enhancing the thermoelectric efficiency of these materials.

3.1.2.3. Electronic thermal conductivity

k_e , the electronic thermal conductivity, is a measure of the heat current that occurs when there is a temperature difference. To create a more advanced material for thermoelectric technology, it is essential to have low thermal conductivity. The electronic contribution to thermal conductivity can be described as follows:

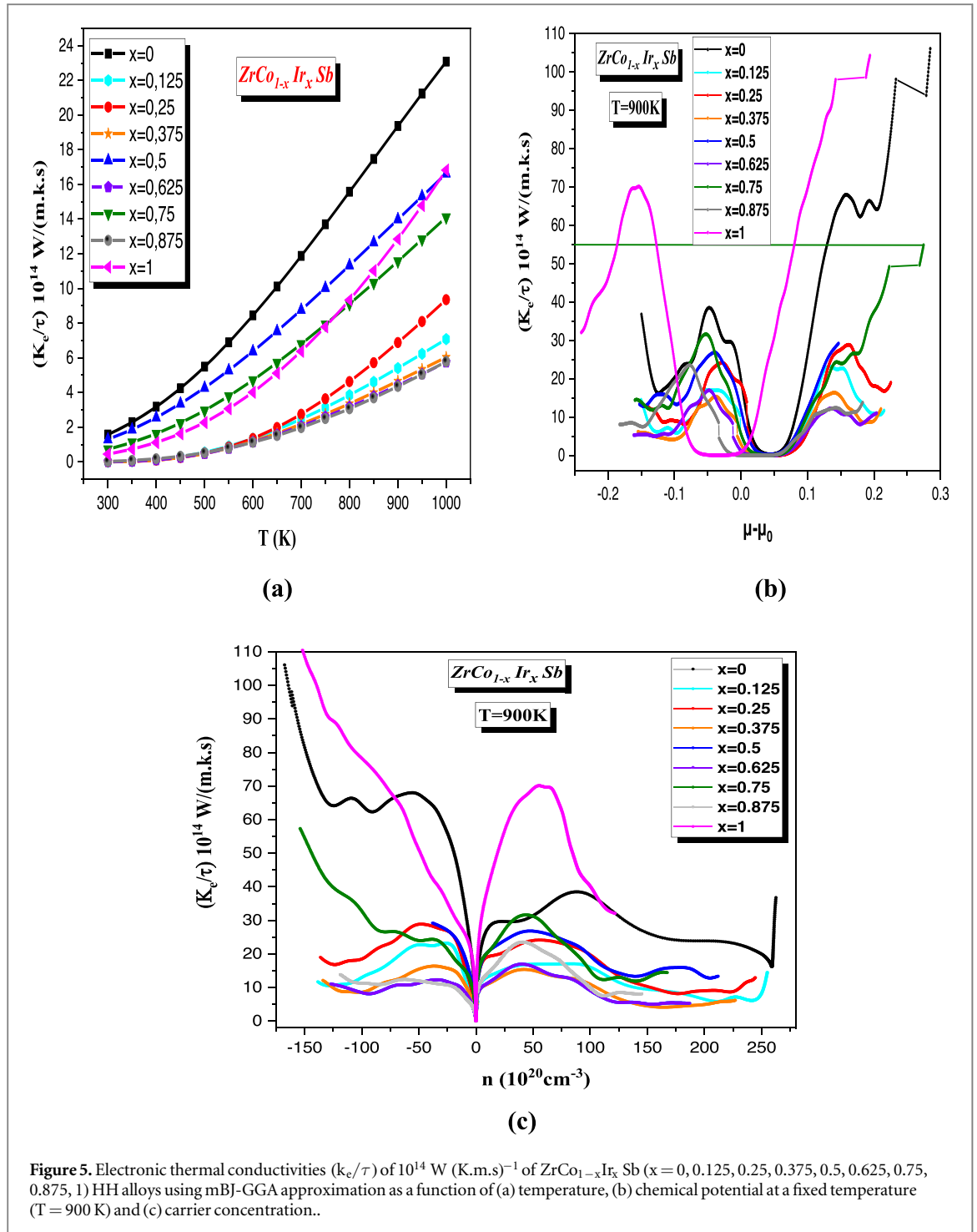
$$k_e = K_B^2 T \sum_k \left(-\frac{\partial f_0}{\partial E} \right) \tau_{\vec{k}} v_{\vec{k}} v_{\vec{k}} \left(\frac{\epsilon_k - \mu}{K_B T} \right)^2 - T \sigma S^2. \quad (10)$$

We also use the Wiedemann–Franz law [63] to determine the electronic thermal conductivity:

$$k_e = \mathcal{L} T \sigma. \quad (11)$$

The Lorenz number is represented by \mathcal{L} . However, \mathcal{L} certain semiconductor thermoelectric materials with heavy doping are extremely near the degenerate limit [65].

Figure 5(a) displays the electronic thermal conductivities (k_e/τ) of $10^{14} W (K.m.s)^{-1}$ for $ZrCo_{1-x}Ir_xSb$ HH alloys throughout a temperature range of 300–1000 K. This figure also shows that k_e/τ for all HH alloys increases with temperature. On the flip side, we observed that the electronic thermal conductivity of almost all alloys—aside from alloys $ZrCoSb$ $ZrCo_{0.5}Ir_{0.5}Sb$ is practically null at room temperature $((k_e/\tau) \sim 0)$. Furthermore, the $ZrCo_{0.625}Ir_{0.375}Sb$ alloy was found to have a lower minimum electronic thermal conductivity



value 0.002×10^{14} W (K.m.s) $^{-1}$ at 300 K than other alloys, which assists in clarifying why it has the highest thermoelectric performance. In addition, the alloys with concentrations of ($x = 0.125, 0.25, 0.375, 0.625$, and 0.875) exhibit the lowest electronic thermal conductivity at high temperatures (1000 K), ranging from 5.74 to 9.34×10^{14} W (K.m.s) $^{-1}$. This further highlights the alloys' high thermoelectric performance.

Figure 5(b) illustrates the variation in electronic thermal conductivity (κ_e/τ) as a function of chemical potential (μ) for the $\text{ZrCo}_{1-x}\text{Ir}_x\text{Sb}$ half-Heusler (HH) alloys at a fixed temperature of 900 K. The graph shows a characteristic trend where κ_e/τ increases with chemical potential across all alloys, reaching a minimal value of 0.018×10^{14} W(K.ms) $^{-1}$ at -0.03 eV for the ZrIrSb alloy. This point marks a region where the thermal transport due to electrons is nearly suppressed, likely due to the low density of states available for conduction near this chemical potential. As μ approaches 0 eV, corresponding to the Fermi level, κ_e/τ becomes nearly zero, indicating the minimal contribution of electronic carriers to thermal conductivity at this energy level. Beyond this, as μ continues to rise, κ_e/τ starts to increase again, reflecting the enhanced thermal transport as more charge carriers are thermally excited into higher energy states. The plot reaches an optimum value of

Table 2. The estimated values of S , k_{total} and ZT of $ZrCo_{1-x}Ir_xSb$ HH alloys at temperatures of 300, 600, and 900 using EV-GGA and mBJ-GGA approximations.

x	T (K)	EV-GGA			mBJ-GGA			Previous calculations		
		S ($\mu V/K$)	k_{total} ($W/m.K$)	ZT	S ($\mu V/K$)	k_{total} ($W/m.K$)	ZT	S ($\mu V/K$)	k_{total} ($W/m.K$)	ZT
0	T = 300	210	16.75	0.13	222	16.60	0.12	130 [34]	22 [9]	0.12 [30]
	T = 600	227	22.94	0.54	235	22.97	0.55	—	—	—
	T = 900	221	41.89	0.70	226	42.34	0.71	—	—	—
0.125	T = 300	211	4.48	0.01	341	4.47	~0			
	T = 600	263	4.52	0.72	270	4.75	0.77			
	T = 900	236	11.29	0.96	237	12.09	0.97			
0.25	T = 300	266	5.75	~0	266	5.77	~0			
	T = 600	290	4.84	0.61	285	5.33	0.68			
	T = 900	273	13.80	1	264	15.35	1.01			
0.375	T = 300	302	3.40	~0	353	3.40	~0			
	T = 600	287	3.57	0.79	280	3.92	0.84			
	T = 900	244	9.42	1	237	10.25	1			
0.5	T = 300	233	11.54	0.13	214	11.92	0.14			
	T = 600	237	15.97	0.56	226	17.04	0.56			
	T = 900	225	29.13	0.71	217	30.58	0.7			
0.625	T = 300	235	3.62	0.02	318	3.67	~0			
	T = 600	256	3.98	0.78	261	15.34	0.2			
	T = 900	289	9.80	0.97	232	53.97	0.17			
0.75	T = 300	211	7.35	0.19	273	6.63	0.16			
	T = 600	232	13.79	0.61	263	11.78	0.63			
	T = 900	223	27.63	0.73	244	24.55	0.76			
0.875	T = 300	57	3.65	~0	73	3.65	~0			
	T = 600	214	3.73	0.66	211	3.91	0.68			
	T = 900	221	9.20	0.91	218	9.71	0.91			
1	T = 300	276	13.04	0.04	281	13.08	0.05	34.4 [65]	9.5 [65]	—
	T = 600	291	13.98	0.44	294	13.56	0.46	—	—	—
	T = 900	285	27.52	0.71	285	29.01	0.72	—	—	—

$70.09 \times 10^{14} \text{ W(K.ms)}^{-1}$ at a chemical potential of -0.15 eV for the $ZrIrSb$ alloy, indicating that at this particular energy level, the balance between the number of carriers and their ability to transport thermal energy is maximized. This behavior highlights the sensitive dependence of electronic thermal conductivity on the position of the chemical potential within the electronic band structure, suggesting potential for fine-tuning κ_e/τ through precise control of doping and carrier concentration to enhance thermoelectric performance.

Figure 5(c) presents the variation of electronic thermal conductivity (κ_e/τ) as a function of carrier concentration for the $ZrCo_{1-x}Ir_xSb$ HH alloys. The plot reveals that the electronic thermal conductivity decreases with increasing carrier concentration for all alloys, reaching its lowest point when the carrier concentration is zero. This trend suggests that at low carrier concentrations, the reduced number of available charge carriers limits the material's ability to conduct heat via electronic means. However, as the carrier concentration continues to increase, κ_e/τ begins to rise again, indicating that a higher density of charge carriers can effectively contribute to the thermal conductivity of the material. Notably, the $ZrIrSb$ alloy achieves an optimum value of $115.55 \times 10^{14} \text{ W(K.ms)}^{-1}$ at a carrier concentration of $-157.47 \times 10^{20} \text{ cm}^{-3}$. This peak value underscores the importance of optimizing carrier concentration to balance electrical and thermal transport properties, which is critical for maximizing the thermoelectric efficiency of the alloy. The observed trends highlight the delicate interplay between carrier concentration and electronic thermal conductivity, suggesting that careful tuning of these parameters can lead to significant improvements in thermoelectric performance.

3.1.2.4. Figure of merit

ZT values around or more prominent than unity are regarded as having good properties for materials used in thermoelectric devices [64, 65]. Table 2 shows that the $ZrCo_{1-x}Ir_xSb$ HH alloys' calculated figure of merit ZT from $x = 0$ to $x = 1$ using the modified Beck-Johnson approximation (mBJ-GGA) agrees well with the previous calculations [31–34]. Figures 6(a)–(d)–(e) illustrates that a maximum ZT of approximately 1.01 was attained $ZrCo_{0.75}Ir_{0.25}Sb$ at 1000 K with a carrier concentration of $n = 1.47 \cdot 10^{20} \text{ cm}^{-3}$ and $ZrCo_{0.625}Ir_{0.375}Sb$ at 800 K with a carrier concentration of $n = 7.23 \cdot 10^{19} \text{ cm}^{-3}$. This is attributed to the greater Seebeck coefficient

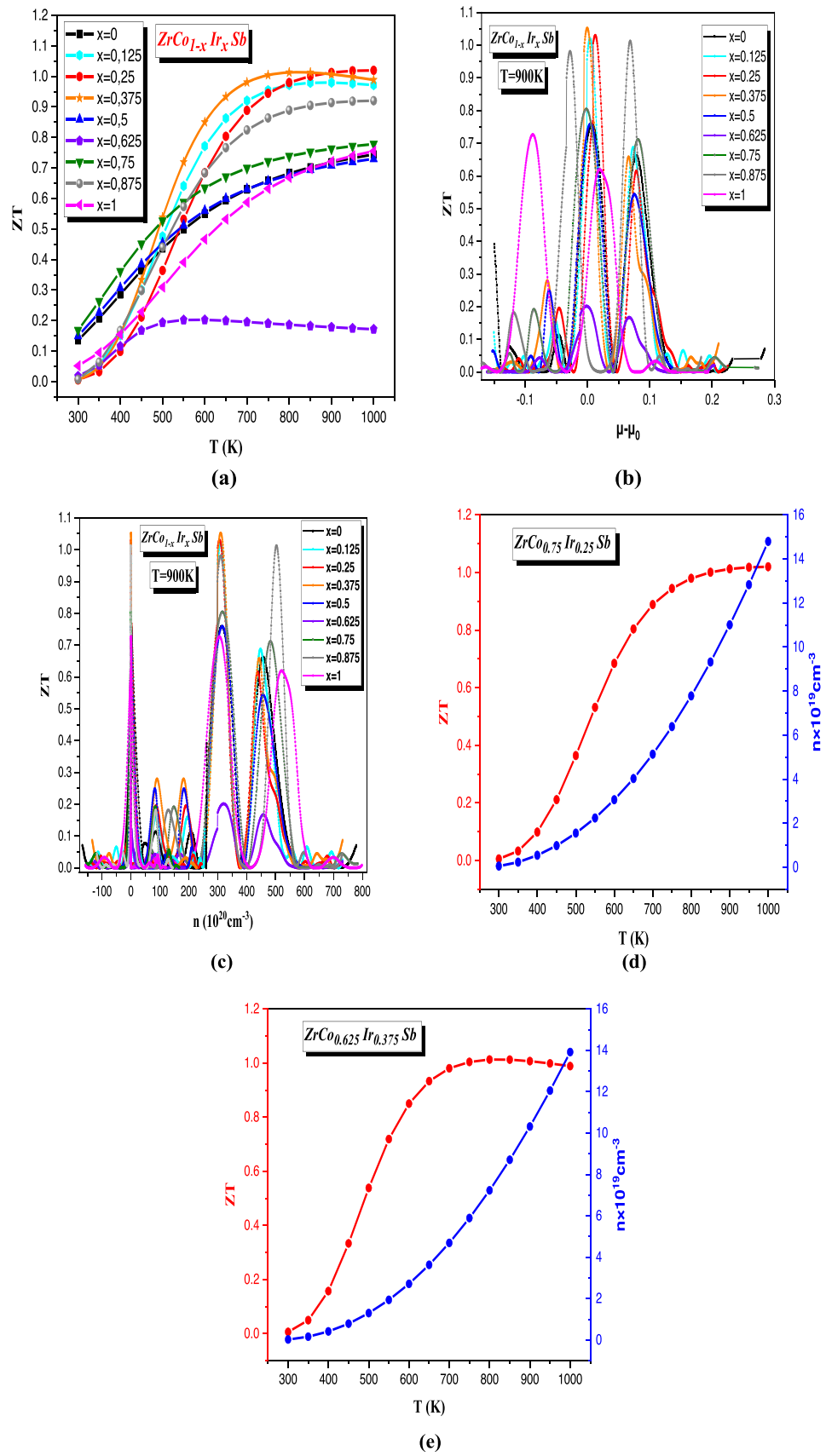


Figure 6. Figure of merit of $\text{ZrCo}_{1-x}\text{Ir}_x\text{Sb}$ ($x = 0, 0.125, 0.25, 0.375, 0.5, 0.625, 0.75, 0.875, 1$) HH alloys using mBJ-GGA approximation as a function of (a) temperature, (b) chemical potential at a fixed temperature ($T = 900\text{ K}$), (c) carrier concentration, temperature and carrier concentration (d) for $\text{ZrCo}_{0.75}\text{Ir}_{0.25}\text{Sb}$ and (e) for $\text{ZrCo}_{0.625}\text{Ir}_{0.375}\text{Sb}$ HH.

values and lower thermal conductivity, as shown in table 2. These findings highlight the latest advancements in HH alloys and surpass the previously documented results for ternary HH alloy [66–76]. It is worth mentioning that in figure 6(a), the increase in HH alloys is more pronounced at higher temperatures. Except for $\text{ZrCo}_{1-x}\text{Ir}_x\text{Sb}$ alloys at concentrations of $x = 0.125$, $x = 0.375$, and $x = 0.625$, the value decreases at 950, 850, and 650, respectively. Nevertheless, according to table 2, the values for $\text{ZrCo}_{1-x}\text{Ir}_x\text{Sb}$ ($x = 0.125, 0.25, 0.375, 0.625$, and 0.875) at room temperature are extremely close to zero. Based on this table, the concentration of $\text{ZrCo}_{0.375}\text{Ir}_{0.625}\text{Sb}$ in the alloy is deficient. The value is less than 0.2. In our earlier publications, we have also computed the ZT values for various thermoelectric materials and provided a detailed analysis of the results. [77–79].

Figures 6(b) and (c) illustrate the variations in the thermoelectric figure of merit (ZT) as functions of chemical potential (μ) and carrier concentration for the $\text{ZrCo}_{1-x}\text{Ir}_x\text{Sb}$ half-Heusler (HH) alloys at a fixed temperature of 900 K. These figures reveal the nuanced relationship between the ZT values and the electronic structure of the alloys, demonstrating their potential as high-temperature thermoelectric semiconductors.

In figure 6(b), the ZT values are plotted against the chemical potential. The graph shows that the ZT value fluctuates as the chemical potential shifts, reflecting the complex interplay between electrical conductivity, Seebeck coefficient, and thermal conductivity within the material. Notably, the $\text{ZrCo}_{0.625}\text{Ir}_{0.375}\text{Sb}$ alloy achieves a peak ZT value of 1.05 at a chemical potential of -5.62×10^{-4} eV. This peak indicates an optimal balance where the electronic properties align to maximize the efficiency of thermoelectric conversion. The location of this peak suggests that even slight adjustments to the chemical potential can significantly impact the thermoelectric performance, emphasizing the need for precise control over doping levels and electronic structure.

Figure 6(c) presents the ZT values as a function of carrier concentration. As seen in the figure, the ZT values exhibit a similar sensitivity to carrier concentration, with the $\text{ZrCo}_{0.625}\text{Ir}_{0.375}\text{Sb}$ alloy again standing out, reaching its maximum ZT value of 1.05 at a carrier concentration of $0.43 \times 10^{20} \text{ cm}^{-3}$. This peak suggests that an optimal carrier concentration exists where the thermoelectric performance is maximized. The ZT value's dependency on carrier concentration highlights the importance of achieving the right balance between carrier mobility and density, which is crucial for enhancing thermoelectric efficiency.

These findings indicate that the $\text{ZrCo}_{0.625}\text{Ir}_{0.375}\text{Sb}$ alloy has a particularly favorable combination of electronic and thermal properties that make it well-suited for high-temperature thermoelectric applications. The ability to fine-tune ZT through adjustments to chemical potential and carrier concentration offers valuable insights into the design and optimization of thermoelectric materials, paving the way for more efficient energy conversion technologies.

4. Conclusion

The thermoelectric transport properties of $\text{ZrCo}_{1-x}\text{Ir}_x\text{Sb}$ ($x = 0, 0.125, 0.25, 0.375, 0.5, 0.625, 0.75, 0.875, 1$) half-Heusler alloys with varying compositions were analyzed using the DFT and Boltzmann transport theories. The overall thermal conductivity closely aligns with the findings from previous calculations. It was discovered that by increasing the concentration of iridium (Ir_x) from $x = 0$ to 0.375 in the $\text{ZrCo}_{1-x}\text{Ir}_x\text{Sb}$ alloys from room temperature to 800 K, there was a notable decrease in thermal and electrical conductivity. This can be attributed to a shorter relaxation time. In order to enhance the thermoelectric performance, decrease in thermal conductivity is crucial for efficient thermoelectric generators. In addition, this work demonstrates that this particular material $\text{ZrCo}_{0.625}\text{Ir}_{0.375}\text{Sb}$ exhibits the highest Seebeck coefficient ($353.93 \mu\text{V/K}$) at 300 K, which significantly enhances its thermoelectric capabilities. Finally, there is a significant increase $\text{ZrCo}_{1-x}\text{Ir}_x\text{Sb}$ for the extensively researched half-Heusler alloys, surpassing the previous maximum for ZrMSb ($M = \text{Co}$ or Ir) ternary alloys of 0.74 or higher. Unexpectedly, we accomplished a substantial increase in thermoelectric properties with a ZT value of 1.01 by applying 25% ($x = 0.25$) of atomic doping of iridium (Ir) with a carrier concentration of $n = 1.47 \cdot 10^{20} \text{ cm}^{-3}$ 1000 K and 37.5% ($x = 0.375$) of atomic doping of iridium (Ir) with a carrier concentration of $n = 7.23 \cdot 10^{19} \text{ cm}^{-3}$ at 800 K. Consequently, we trust that these alloys will make excellent thermoelectric application candidates.

The investigation of $\text{ZrCo}_{1-x}\text{Ir}_x\text{Sb}$ half-Heusler alloys and their thermoelectric properties presents significant potential for practical applications in various fields. The alloys studied, particularly with $x = 0.25$, demonstrate a high thermoelectric figure of merit (ZT) of 1.01 at 1000 K. This promising performance underscores the suitability of these materials for several key applications:

1. **Waste heat recovery:** These alloys can effectively convert waste heat from industrial processes, automotive exhausts, and power generation systems into electrical energy. This application is crucial for improving energy efficiency and reducing greenhouse gas emissions by harnessing otherwise wasted thermal energy.

2. **Power generation:** In remote or off-grid locations, where conventional power sources may be limited, these materials can be utilized in thermoelectric generators to provide a reliable source of electricity by exploiting temperature gradients.
3. **Cooling systems:** The efficiency of these alloys in thermoelectric applications also extends to cooling technologies. Their ability to manage and dissipate heat makes them suitable for cooling electronics, refrigeration systems, and air conditioning units, offering a solid-state alternative to traditional cooling methods.
4. **Wearable electronics:** The capability to convert body heat into electrical energy presents opportunities for powering wearable devices and sensors. This advancement can contribute to the development of innovative health monitoring systems and enhance the functionality of IoT-enabled wearable technologies.

By showcasing the broad range of applications enabled by the thermoelectric properties of $\text{ZrCo}_{1-x}\text{Ir}_x\text{Sb}$ alloys, this work emphasizes the material's potential impact on energy efficiency, power generation, thermal management, and wearable technology.

Acknowledgments

All authors would like to thank the general directorate for scientific research and technological development for their financial support during the realization of this work.

Data availability statement

All data that support the findings of this study are included within the article (and any supplementary files).

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